

Fourier Series $f(t) \approx \frac{a_0}{2} + \sum_{n=1}^{\infty} a_n \cos\left(\frac{2\pi n t}{T}\right) + \sum_{n=1}^{\infty} b_n \sin\left(\frac{2\pi n t}{T}\right)$

$a_0 = \frac{1}{T} \int_{-T/2}^{T/2} f(t) dt$; $a_n = \frac{1}{T} \int_{-T/2}^{T/2} f(t) \cos\left(\frac{2\pi n t}{T}\right) dt$

$\sum \cos(\omega t - \theta) = A \cos(\omega t) + B \sin(\omega t)$ $A = X \cos \theta$
 $\sum \sin(\omega t - \theta) = A \cos(\omega t) + B \sin(\omega t - \pi/2)$ $B = X \sin \theta$ $\theta = \tan^{-1} \frac{B}{A}$

$\cos x = 1 - \frac{x^2}{2} + \frac{x^4}{4!} - \dots$; $\sin x = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \dots$

$\sin^2 x = \frac{1}{2} - \frac{1}{2} \cos 2x$ $\sin u \sin v = \frac{1}{2} [\cos(u-v) - \cos(u+v)]$

$\cos^2 x = \frac{1}{2} + \frac{1}{2} \cos 2x$ $\cos u \cos v = \frac{1}{2} [\cos(u-v) + \cos(u+v)]$

$\sin 2x = 2 \sin x \cos x$ $\sin u \cos v = \frac{1}{2} [\sin(u+v) + \sin(u-v)]$

$\cos 2x = 1 - 2 \sin^2 x$

Complex F.S. $f(t) \sim \sum_{n=-\infty}^{\infty} C_n e^{j \frac{2\pi n t}{T}} = \sum_{n=-\infty}^{\infty} C_n e^{j n \omega t}$; $C_n = \frac{1}{T} \int_{-T/2}^{T/2} f(t) e^{-j n \omega t} dt$

$a_n = C_n + C_{-n}$

$b_n = j(C_n - C_{-n})$

$a_0 = 2C_0$

Critical damping $x(t) = e^{-\omega_n t} (C_1 + C_2 t)$ see slide 165

$C_1 = x_0$

$C_2 = \dot{x}_0 + \omega_n x_0$

$C_{critical} = 2m\omega_n$; $\zeta = \frac{c}{c_r} = \frac{c}{2m\omega_n}$

$\ddot{x} + 2\zeta\omega_n \dot{x} + \omega_n^2 x = F$, $\omega_n = \sqrt{\frac{k}{m}}$, $2\zeta\omega_n = \frac{c}{m}$, $\zeta = \frac{c}{2\sqrt{km}}$

Undamped: $x(t) = x_0 \cos \omega_n t + \frac{\dot{x}_0}{\omega_n} \sin \omega_n t$ or $x(t) = X \cos(\omega_n t - \theta)$

damped: $\zeta > 1$ $x(t) = e^{-\omega_n t} [x_0 + (\dot{x}_0 + \omega_n x_0) t]$ $X = \sqrt{x_0^2 + \left(\frac{\dot{x}_0}{\omega_n}\right)^2}$; $\theta = \tan^{-1} \left(\frac{\dot{x}_0}{\omega_n x_0}\right)$

$\zeta < 1$ $x(t) = e^{-\zeta\omega_n t} (A \cos(\omega_d t) + B \sin(\omega_d t))$. $A = x_0$; $B = \frac{\dot{x}_0 + \zeta\omega_n x_0}{\omega_d}$

$\omega_d = \omega_n \sqrt{1 - \zeta^2}$ or $x(t) = X e^{-\zeta\omega_n t} \cos(\omega_d t - \phi)$; $X = \sqrt{A^2 + B^2}$, $\phi = \tan^{-1} \left(\frac{B}{A}\right)$

Log decrement $\ln\left(\frac{x_1}{x_2}\right) = \zeta\omega_n T_d$ must be over one period

$= \frac{2\pi\zeta}{\sqrt{1-\zeta^2}} = \delta$. if more than one cycle is given then

$\delta = \frac{1}{n} \ln\left(\frac{x_1}{x_{n+1}}\right)$ Find δ . then \uparrow to find ζ . Then find $\omega_n = \frac{2\pi}{T\sqrt{1-\zeta^2}}$. Find ω_n

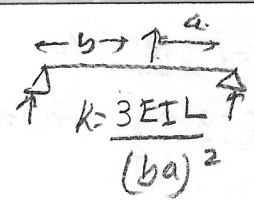
For rotation $C_{critical} = 2I_0 \omega_n$

For critical damping, $x_{max} = \frac{\dot{x}_0 e^{-t}}{\omega_n}$

For beads use $m = 0.229$ column mass
 for longitudinal \uparrow use $\frac{1}{3}$ mass of spring

Stiffness

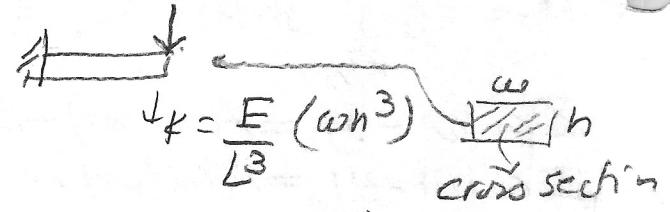
$k = \frac{AE}{L}$; $k = 3EI \left(\frac{L}{ab}\right)^3$



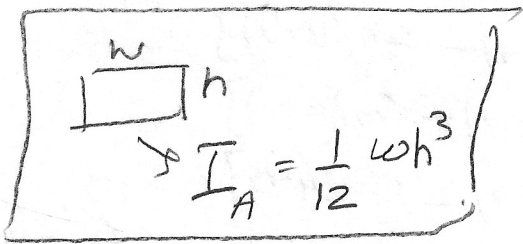
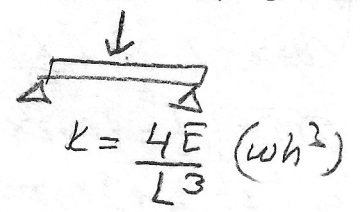
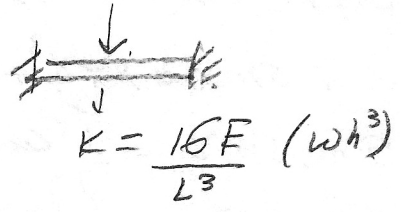
10mm = 0.0625 in. $\frac{2R}{L}$

slide 24

$k = \frac{Gd^4}{64nR^3}$

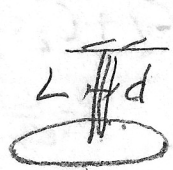


$EA = kL$

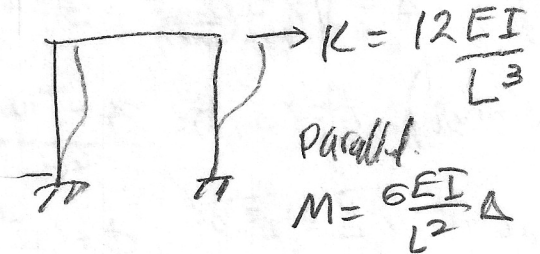
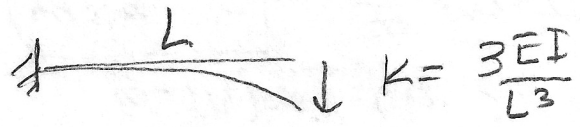


$KE = \frac{1}{2}mv^2 + \frac{1}{2}I_{cg}\dot{\theta}^2$ or $\left(\frac{1}{2}I_0\dot{\theta}^2\right)$

Torsion



$k_t = \frac{T}{\theta} = \frac{GI_0}{L} = \frac{\pi Gd^4}{32L}$. $I_0 = \frac{\pi d^4}{32}$



$G = \frac{6EI}{L^2 S}$

$X_p = \frac{1}{1-r^2} \sin \omega t$ for $r < 1$

$X_p = \frac{1}{r^2-1} \sin \omega t$ for $r > 1$

unbalance
 $m\ddot{x} + kx = m_0 e^{\omega^2} \sin \omega t$
 free damp.
 resona $\omega = \omega_n$
 $\omega_r = \omega_n \sqrt{1-2\zeta^2}$
 $\omega_r < \omega_d < \omega_n$

$\frac{1}{\sqrt{1-r^2}} = \frac{1}{r^2-1}$ for $r > 1$
 $\frac{1}{1-r^2}$ for $r < 1$

impulse response
 $x(t) = \frac{\int \hat{F} dt}{m\omega_n} \sin \omega_n t$
 use $m\dot{v} = \int \hat{F} dt$ to find $\dot{x}(t)$

$I_0 = \frac{\pi d^4}{32}$. Polar moment of inertia
 $\theta = \frac{(Torsion)(L)}{GI_0}$

$\int \hat{F} dt = m\dot{v}(t)$ assume $v(0) = 0$

given: $m\ddot{x} + Kx = f$.

① Find $A = M^{-1}K$. ② Find λ_1, λ_2 .

③ find eigenvectors $u_1, u_2 \Rightarrow [u]$

④ write $\{\ddot{q}\} + \begin{bmatrix} \omega_1^2 & 0 \\ 0 & \omega_2^2 \end{bmatrix} \{q\} = \bar{u}^{-1} M^{-1} \{f\}$.

⑤ solve these.

⑥ let $x = [u]\{q\} \Rightarrow q(0) = \bar{u}^{-1} x(0)$.

⑦ transfer back to normal coordinates.

for damped system. use slide

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$$[M]\ddot{q} + \beta[M]\Omega\dot{q} + M\Omega^2q = \bar{u}^T f$$

$$\text{where } [M] = \bar{u}^T m u, \text{ and } \Omega = \begin{bmatrix} \omega_1 & 0 \\ 0 & \omega_2 \end{bmatrix}$$

For beam problems, easier to use Flexibility
For spring problems, easier to use stiffness

$$a\lambda^2 + b\lambda + c = 0 \Rightarrow \lambda = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} \text{ eigenvalues}$$

one mile = 5280 ft.

one mile = 1609.34 meters

$$\begin{bmatrix} a & b \\ c & d \end{bmatrix}^{-1} = \frac{1}{\det(A)} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$$