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Course: MAE 91

Set: #2

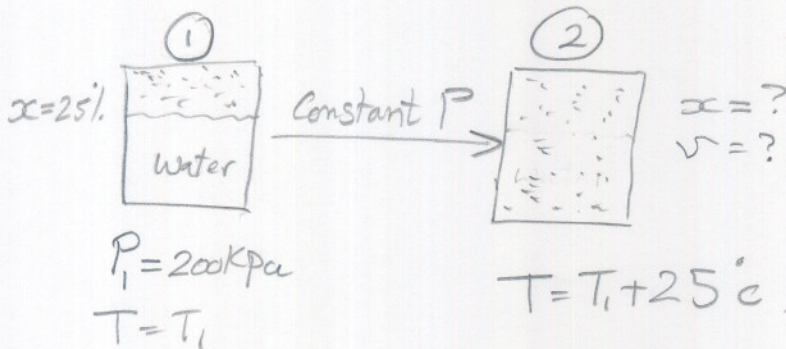
date: July 13, 2004

138/140

### Problem 3.14

#### 19/10 statement

given water at 200 kPa,  $x = 25\%$  (i.e. mass of water is 75% of the control mass total). Now temp is raised by  $20^\circ\text{C}$  in constant pressure process. Find new quality and new Volume.



Given  
 $x_1, P_1, P_2, \Delta T = 20^\circ\text{C}$

Find  
 $x_2, v_2$

#### assumptions

Pure substance.

ideal process (quasi-equilibrium process)

#### Laws

$$v = v_f + x(v_g - v_f)$$

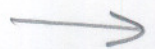
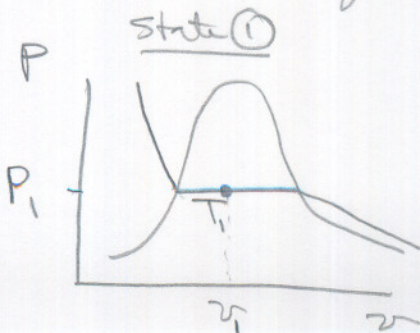
IF  $T > T_{\text{saturation}}$  at constant  $P \Rightarrow$  superheated vapor state!

#### steps

Find specific volume in state ①

$$v_1 = v_f + x(v_g - v_f)$$

Since  $P$  is given, we can look up from Table B.1.2 (Saturated water pressure table) to find, at  $P = 200 \text{ kPa}$  the values for  $v_f, v_g$ . also we find  $T_{1(\text{sat})}$  from same entry.



T in state 2 is  $T_2$

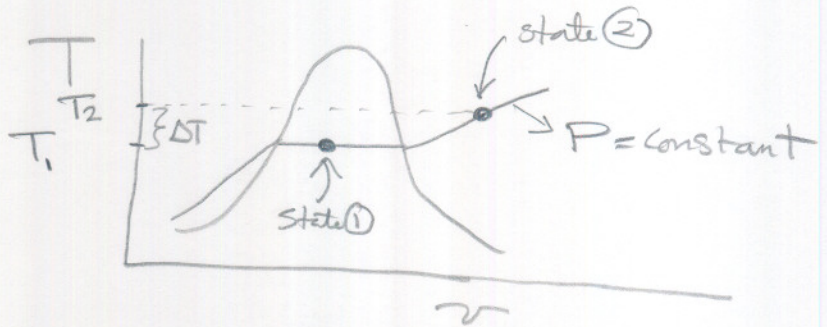
where  $T_2 = T_1 + \Delta T$

Since P is constant, and  $T_2 > T_1$ , we are in superheated vapor state.

so  $x_2$  is undefined

to find  $v_2$ , use Table B.1.3 (superheated vapor water Table).

need to use interpolation here.



### Numerical

From Table B.1.2, for  $P=200 \text{ kPa}$ ,  $v_f = 0.001061$ ,  $v_g = 0.88573$   
but  $x_1 = 0.25$

hence  $v_{\text{State 1}} = v_f + x(v_g - v_f) = 0.001061 + 0.25(0.88573 - 0.001061)$   
 $= 0.222228 \text{ m}^3/\text{kg}$

$$T_2 = T_1 + \Delta T$$

$$T_2 = 120.23 + 20 = 140.23 \text{ }^\circ\text{C}$$

From Table B.1.2 for  $P=200 \text{ kPa}$ .

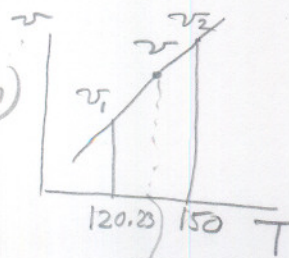
hence  $x_2$  undefined

from Table B.1.3 (superheated vapor). from book for  $P=200 \text{ kPa}$

we see that  $v_{1, \text{super}} = 0.88573$ ,  $v_2 = 0.95964$

$$\text{so } \frac{v - v_1}{20} = \frac{v_2 - v_1}{150 - 120.23} \Rightarrow v =$$

$$v = 20 \frac{(0.95964 - 0.88573)}{150 - 120.23} + 0.88573 = 0.93538 \text{ m}^3/\text{kg}$$



so  $v$  changed from  $v_{\text{State 1}} = 0.2223 \text{ m}^3/\text{kg}$  to  $v_{\text{State 2}} = 0.9354 \text{ m}^3/\text{kg}$

### Problem 3.32

10/16 Determine whether R-22 in each of following state is in a compressed liquid, superheated vapor, or saturated liquid and vapor.

a)  $50^\circ\text{C}$ ,  $v = 0.05 \text{ m}^3/\text{kg}$

b)  $1 \text{ MPa}$ ,  $20^\circ\text{C}$

c)  $0.1 \text{ MPa}$ ,  $0.1 \text{ m}^3/\text{kg}$

d)  $-20^\circ\text{C}$ ,  $200 \text{ kPa}$ .

So, we are given 2 properties in each state. from these 2 properties, we look up from Table to find the state.

#### Assumptions

System in equilibrium.

#### Laws

use R-22 Tables. (B.4.1, B.4.2)

← saturated ← superheated.

#### Steps

- From B.4.1 look up entry of  $v_f, v_g$  for  $T$ , and determine where given  $v$  is located.
- From B.4.1, lookup  $P_{\text{sat}}$  for given  $T = 20^\circ\text{C}$ . compare if  $P$  in Table is less than or greater than  $1 \text{ MPa}$ . This tells the phase.
- From B.4.1, look up  $v_f, v_g$  for given  $P$  ( $0.1 \text{ MPa}$ ) and compare given  $v$  to see which phase.
- From table B.4.1, for given  $T = -20^\circ\text{C}$ , look up  $P_{\text{sat}}$  and compare to given  $P$  to determine phase.



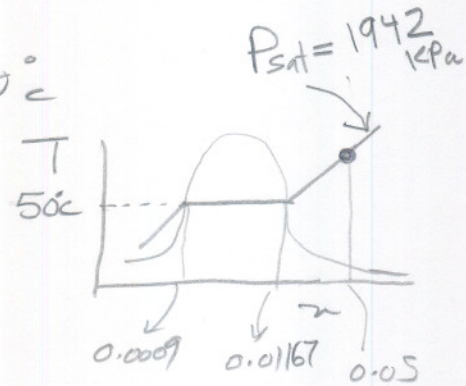
## Numerical

a) From Table B.4.1, for  $T = 50^\circ\text{C}$

$$v_f = 0.000922, \quad v_g = 0.01167$$

but  $v = 0.05 \text{ m}^3/\text{kg}$

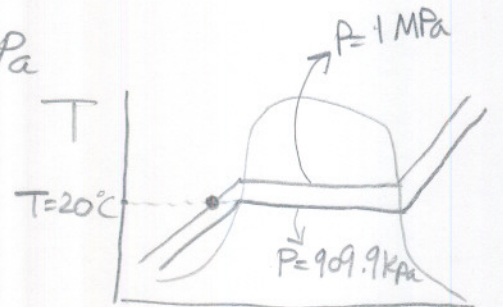
So, Super heated Vapor



b) from B.4.1.

For  $T = 20^\circ\text{C}$ ,  $P_{\text{sat}} = 909.9 \text{ kPa}$   
 but since  $P > P_{\text{sat}}$ .

hence in Compressed liquid

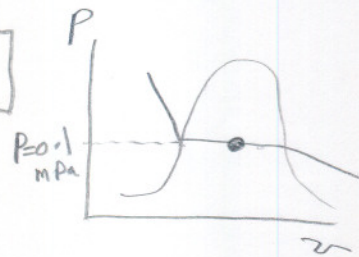


c) From B.4.1, for  $P = 0.1 \text{ MPa}$ , this entry in second column does not exist, but  $P = 101.3 \text{ kPa}$  is almost  $0.1 \text{ MPa}$ , so for  $P = 101.3 \text{ kPa}$ ,

$$v_f = 0.000708, \quad v_g = 0.21261 \text{ m}^3/\text{kg}$$

so  $v$  given which is  $0.1 \text{ m}^3/\text{kg}$  is between  $v_f$  and  $v_g$

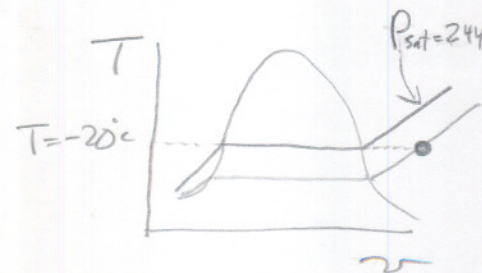
hence Saturated liquid and vapor



d) From B.4.1, for  $T = -20^\circ\text{C}$ ,  $P_{\text{sat}} = 244.8 \text{ kPa}$ .

Since  $P_{\text{given}} > P_{\text{sat}}$ , we see

That R22 is in Super heated Vapor



## Problem 3.33

Statement we are given a table and asked to fill it  
10/10 in. we will use the tables for water to do this.  
in each entry, we are given 2 properties. this is  
the table

	P (kPa)	T (°C)	v [m <sup>3</sup> /kg]	x
a	500	20	?	?
b	500	?	0.2	?
c	1400	200	?	?
d	?	300	?	0.8.

### assumptions

Pure substance in equilibrium.

### Laws

use tables B.1.1, B.1.2, B.1.3,  $v = v_f + x(v_g - v_f)$

IF  $v < v_g \Rightarrow$  solid. IF  $v > v_g \Rightarrow$  superheated.

### steps

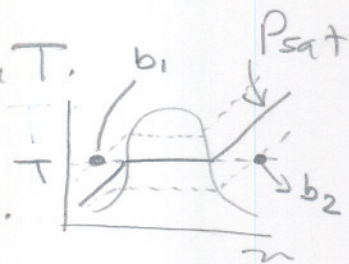
a) we can use table B.1.1 or B.1.2.

use table B.1.1. lookup  $P_{sat}$  for given T.

if  $P_{sat} < P_{given}$  then intersection  
Point  $b_1$  will occur in the solid phase.

IF  $P_{sat} > P_{given}$ , then intersection point  
 $b_2$  will occur in the superheated phase.

if  $P_{sat} = P_{given}$ , then in liquid-vapor phase.



b) After we know which Phase, we can now use  
table B.1.4 (compressed liquid) or B.1.3 (superheated)  
to find v.



b) use B.1.2 (Saturated water pressure table) to find  $v_f, v_g$  for given P. compare given  $v$  to these to determine which phase. if  $v < v_f$  then solid. if  $v > v_g$  then superheated. else mixed phase. depending on the phase, use table B.1.3 (superheated) to lookup T for given P, or use table B.1.4 to lookup T for given P, or use B.1.2 to lookup T for given P if in mixed phase.

$x$  is undefined if in solid or superheated.  
else  $x$  is found from  $v = v_f + x(v_g - v_f)$ .

- c) use same steps as a).  
d) since  $x$  is defined, we know we are in mixed liquid-vapor. so use table B.1.1 to lookup  $P_{sat}$  and  $v_f, v_g$ . then find  $v = v_f + x(v_g - v_f)$ .

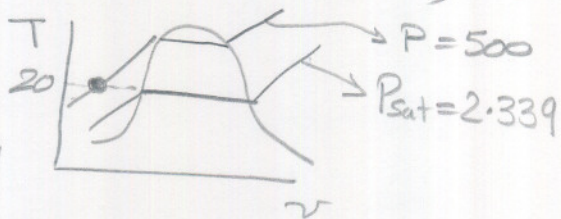
### Numerical

a) From table B.1.1,  $P_{sat} = 2.339$  kPa, but given  $P = 500$  kPa.

so  $P > P_{sat}$

hence in liquid phase.

hence  $x$  undefined



since in liquid phase, then use table B.1.4. For  $P = 500$  kPa lookup for  $T = 20 \Rightarrow v = 0.001002$  m<sup>3</sup>/kg

b) From Table B.1.2, For  $P = 500$  kPa  $\Rightarrow v_f = 0.001093$  m<sup>3</sup>/kg,  $v_g = 0.37489$  m<sup>3</sup>/kg. we are given  $v = 0.2$  m<sup>3</sup>/kg. Hence in mixed liquid-vapor phase.  
so from  $v = v_f + x(v_g - v_f) \Rightarrow \frac{v - v_f}{v_g - v_f} = x \Rightarrow x = \frac{0.2 - 0.001093}{0.37489 - 0.001093}$

$\Rightarrow x = 0.5321$  .  $T_{sat} = 151.86^\circ\text{C}$  From same table B.1.2

since in saturated water - saturated vapor phase.

c) From Table B.1.1, look up  $P_{sat}$  for given  $T=200^\circ\text{C}$ . we find  $P_{sat} = 1553.8 \text{ kPa}$ . As in step (a), we see here that  $P_{sat} > P_{given}$ . hence in super heated vapor phase

hence  $x$  undefined



to find  $v$ , now use table B.1.3

Since  $P_{given}$  is  $1400 \text{ kPa}$ , use table for  $P=1400 \text{ kPa}$ , entry for  $T=200^\circ\text{C} \Rightarrow v = 0.14302 \text{ m}^3/\text{kg}$ .

d) since  $x$  is defined, this is mixed liquid-vapor phase.

From Table B.1.1, lookup  $P_{sat}$  for  $T=300^\circ\text{C}$ .

$\Rightarrow P_{sat} = 8581.0 \text{ kPa}$ .  $\Rightarrow v_f = 0.001404 \text{ m}^3/\text{kg}, v_g = 0.02167 \text{ m}^3/\text{kg}$

$v = v_f + x(v_g - v_f) \Rightarrow v = 0.001404 + 0.8(0.02167 - 0.001404)$

$\Rightarrow v = 0.0176168 \text{ m}^3/\text{kg}$

So Final Table is

	P (kPa)	T ( $^\circ\text{C}$ )	$v$ ( $\text{m}^3/\text{kg}$ )	$x$
a	500	20	0.001002	undefined
b	500	151.86	0.2	0.532
c	1400	200	0.14302	undefined
d	8581	300	0.01762	0.8



## Problem 3.34

Statement Place the 4 states a-d listed in Problem 3.33 as labeled dots in a sketch of P-v and T-v diagrams.

Here we are asked to use P-v and T-v and result of Problem 3.33 to locate the states.

assumptions

Pure substance in equilibrium

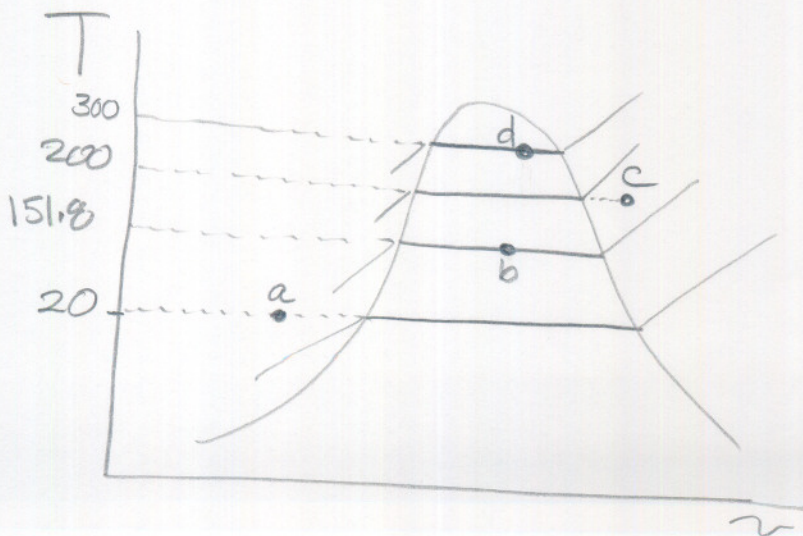
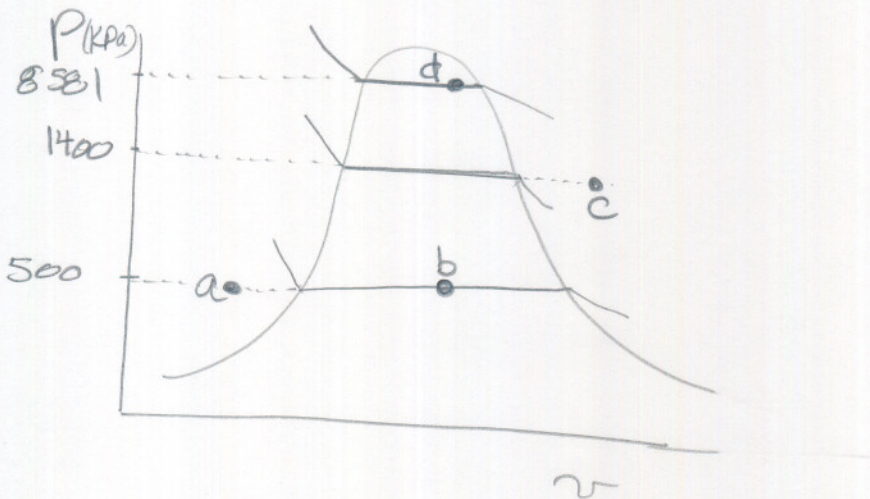
Laws

P-v, T-v diagrams.

steps

draw P-v diagram. Then use result of 3.33 to locate state in diagram. similarly for T-v diagram.

Numerical



### Problem 3.36

Statement give phase and specific volume for the following:

10/16

a. R22,  $T = -25^\circ\text{C}$ ,  $P = 100\text{ kPa}$

b. R22,  $T = -25^\circ\text{C}$ ,  $P = 300\text{ kPa}$

c. R12,  $T = 5^\circ\text{C}$ ,  $P = 200\text{ kPa}$

here we are given 2 properties ( $P, T$ ) and from these need to determine additional property ( $v$ ) and the phase.

#### Assumptions

Pure substance. In equilibrium.

For compressed liquid  $v$ , assume  $v = v_f$ .

#### Laws

use  $T-v$  diagram.

IF  $P_{\text{sat}} > P \Rightarrow$  superheated. IF  $P_{\text{sat}} < P \Rightarrow$  liquid phase.

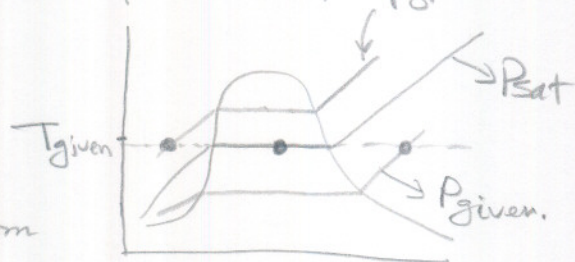
#### Steps

For a, b, c, follow these steps:

From table B.4.1, for given  $T$  find  $P_{\text{sat}}$ ,  $P_{\text{given}}$ .

Then compare  $P_{\text{sat}}$  with  $P_{\text{given}}$ .

IF  $P_{\text{sat}} > P_{\text{given}}$  then R22 is in superheated phase as seen from diagram.



IF  $P_{\text{sat}} < P_{\text{given}}$ , then in liquid phase.

IF  $P_{\text{sat}} = P_{\text{given}}$ , then in mixed liquid-vapor phase.

then depending on phase, use B.4.2 (for superheated) or B.4.1 for saturated or liquid. (take  $v = v_f$  if liquid phase.)

For Part c, use Table B.3.1, B.3.2. and follow same logic as above.  $\rightarrow$

## Numerical

a) From table B.4.1

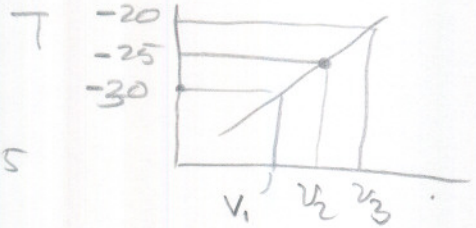
$$T = -25^{\circ}\text{C} \Rightarrow P_{\text{sat}} = 201.0 \text{ kPa.}$$

hence  $P_{\text{sat}} > (P_{\text{given}} = 100)$ .  $\Rightarrow$  superheated Phase

So from table B.4.2, For entry for  $P = 100 \text{ kPa}$ , use interpolation to find  $v$  for  $T = -25^{\circ}\text{C}$ .

we want to find  $v_2$ .

$$\text{so } \frac{(-20) - (-30)}{0.23706 - 0.22675} = \frac{(-25) - (-30)}{v_2 - 0.22675}$$



$$\Rightarrow v_2 = \frac{10}{0.23706 - 0.22675} = \frac{5}{v_2 - 0.22675}$$

$$10v_2 - 2.2675 = 5(0.23706 - 0.22675)$$

$$v_2 = \frac{5(0.23706 - 0.22675) + 2.2675}{10} = \boxed{0.231905 \text{ m}^3/\text{kg}}$$

b) From Table B.4.1

$$T = -25^{\circ}\text{C} \Rightarrow P_{\text{sat}} = 201.0 \text{ kPa}$$

so  $P_{\text{sat}} < (P_{\text{given}} = 300 \text{ kPa})$ .  $\Rightarrow$  liquid Phase

hence use  $v = v_f$ .  $\Rightarrow$   $v = 0.000733 \text{ m}^3/\text{kg}$

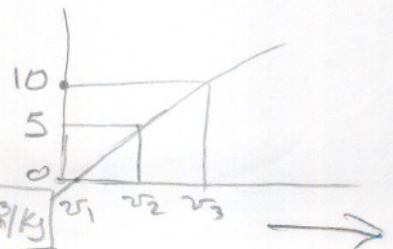
c) From Table B.3.1

$$T = 5^{\circ}\text{C} \Rightarrow P_{\text{sat}} = 362.6 \text{ kPa.}$$

so  $P_{\text{sat}} > P_{\text{given}} \Rightarrow$  superheated vapour

So use table B.3.2. From subtable for  $P = 200 \text{ kPa}$  use interpolation

$$\frac{10 - 0}{0.09255 - 0.08861} = \frac{5 - 0}{v_2 - 0.08861}$$



$$\Rightarrow 10v_2 - 0.8861 = 5(0.09255 - 0.08861)$$

$$v_2 = \frac{5(0.09255 - 0.08861) + 0.8861}{10} = \boxed{0.09058 \text{ m}^3/\text{kg}}$$

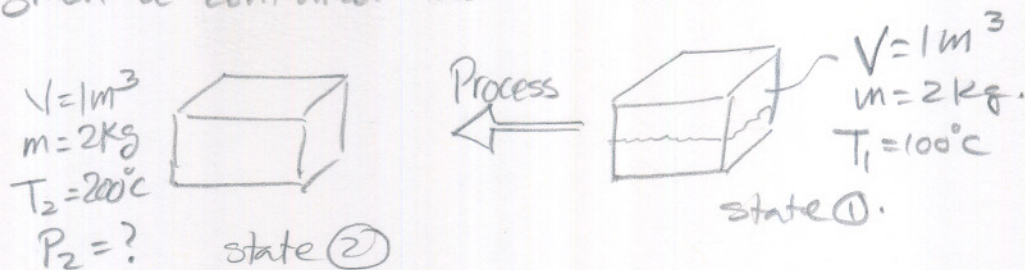
So, summary result:

	Phase	$v$ m <sup>3</sup> /kg
a	superheated vapor	0.231905
b	liquid	0.00073
c	superheated	0.09058

### Problem 3.41

Statement A sealed rigid vessel has  $V=1\text{m}^3$ , contains 2Kg of water at  $100^\circ\text{C}$ . Vessel is now heated. If safety pressure valve is installed, at what Pressure should valve be set to have a max. temp of  $200^\circ\text{C}$ ?

here we are given a controlled mass. we have 2 states.



temp was increased from state ①, and need to find P in state ②.

#### Assumption

Pure Substance.

Ideal process (quasi-equilibrium process)

#### Laws

$v = \frac{V}{m}$ , constant  $v$  process.

#### Steps

Since  $V$  is fixed, and mass is controlled, then  $v$  is constant.  $\boxed{v = \frac{V}{m}} \quad \text{--- (1)}$

From table B.1.1, we look up entry for  $T_1$ , check if supplied  $v$  is  $< v_f$  or  $> v_g$  or in between.

This gives Phase in state ①.

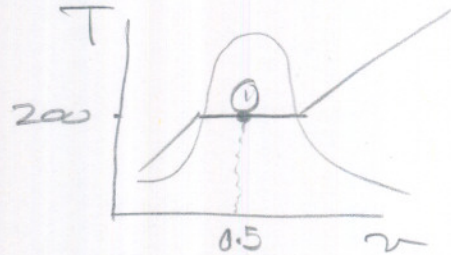
From table B.1.1. we lookup entry for  $T_2$ . again since  $v$  is constant, we can find Phase by comparing to  $v_f$  and  $v_g$ . by knowing phase in state ②, use B.1.3 or B.1.4 to find P for  $T_2$  at this  $v$ .



## Numerical

$$v = \frac{V}{m} = \frac{1}{2} = \boxed{0.5 \text{ m}^3/\text{kg}}$$

From B.1.1 (saturated water),  $v_f = 0.001044 \text{ m}^3/\text{kg}$   
 $v_g = 1.6729 \text{ m}^3/\text{kg}$ .  $\Rightarrow$  mixed liquid-vapor phase



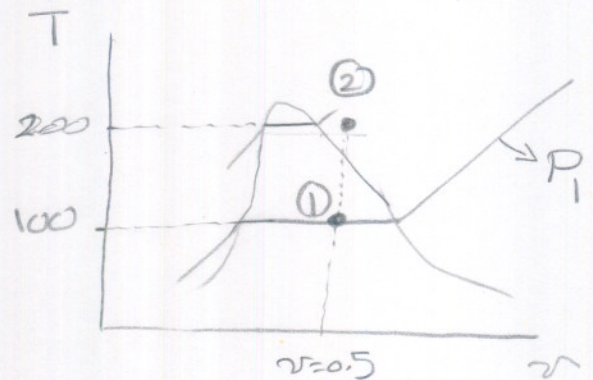
again, from B.1.1, for  $T=200^\circ\text{C}$ ,  $v_f = 0.001156 \text{ m}^3/\text{kg}$ .

$v_g = 0.12736 \text{ m}^3/\text{kg}$ .  $\Rightarrow v > v_g$  in **Superheated Vapor**

Since in superheated phase,  
use table B.1.3

looking at B.1.3, I see that  
at 400 kPa, for  $T=200$ ,  $v=0.53422$ .  
and at 500 kPa,  $T=200$ ,  $v=0.42492$ .

$$\Rightarrow \boxed{400 \text{ kPa} < P_2 < 500 \text{ kPa}}$$

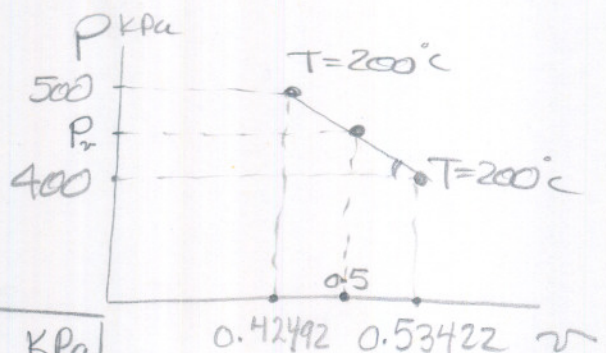


To find correct  $P_2$ , use interpolation.

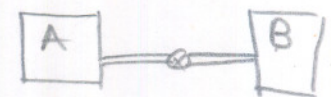
$$\text{so } \frac{500-400}{0.53422-0.42492} = \frac{P_2-400}{0.53422-0.5}$$

$$(P_2-400)(0.53422-0.42492) = 100(0.03422)$$

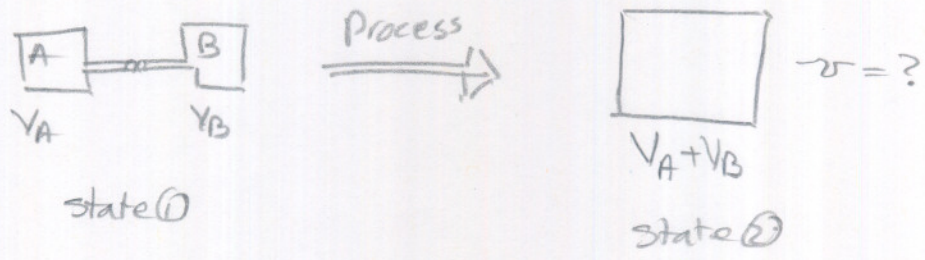
$$P = \frac{3.422}{0.53422-0.42492} + 400 = \boxed{431.308 \text{ kPa}}$$



Problem 3.49 10/10

statement two tanks are connected  tank A at  $P_A = 200 \text{ kPa}$ ,  $v_A = 0.5 \text{ m}^3/\text{kg}$ ,  $V_A = 1 \text{ m}^3$ . tank B contains  $m_B = 3.5 \text{ kg}$ ,  $P_B = 0.5 \text{ MPa}$ ,  $T_B = 400^\circ\text{C}$ . Valve is opened. Find Final state specific Volume.

here we are given an initial state (Valve closed), and Final state (Valve open):



assumptions

Pure Substances, ideal process.

Final Volume =  $V_A + V_B$ , ignore Volume of Pipe connecting 2 tanks.

Laws

$v = \frac{V}{m}$ , tables B.1

since controlled mass and Volume,  $v_{A+B} = \frac{V_A + V_B}{m_A + m_B}$

steps

First analyse state ① Find  $m_A$  from given properties of tank A.

next find  $V_B$  from given properties of tank B.

hence 
$$v_{\text{Final}} = \frac{V_A + V_B}{m_A + m_B}$$

Numerical

From B.1.1, for tank A, at  $P = 200 \text{ kPa} \Rightarrow v_f < v < v_g$ . hence in mixed phase.

$m_A = \frac{V_A}{v_A} = \frac{1}{0.5} = \boxed{2 \text{ kg}}$

For tank B, still in initial state. From B.1.1, we see that for  $P = 0.5 \text{ MPa}$ ,  $T_{\text{sat}} = 151.86^\circ \Rightarrow$  Superheated Vapor. so use B.1.3. For  $P = 0.5 \text{ MPa}$  and  $T = 400^\circ\text{C} \Rightarrow v_B = 0.61728 \frac{\text{m}^3}{\text{kg}}$

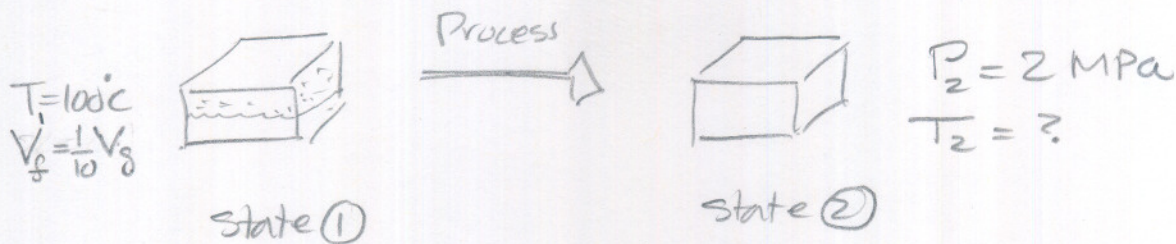
hence  $V_B = v_B m_B = (0.61728)(3.5) = \boxed{2.16048 \text{ m}^3}$

so  $v_{\text{final}} = \frac{V_A + V_B}{m_A + m_B} = \frac{1 + 2.16048}{2 + 3.5} \Rightarrow \boxed{0.57463 \text{ m}^3/\text{kg}}$

# Problem 3.61

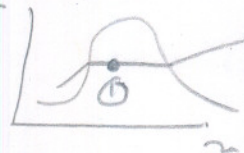
## Statement

a/10 Pressure cooker (closed tank) contains water at  $100^\circ\text{C}$ , with liquid volume at  $1/10$  of vapour volume. It is heated until pressure reaches  $2\text{ MPa}$ . Find final  $T$ . Has final state more or less vapor than initial state?



We are given 2 properties in state ①,  $T$  and  $x$ . So we know already we are in mixed phase.

-1 Show process  $T$



For state ②, we are given one property,  $P$ , and asked to find second independent property  $T$ . Also need to find if in state 2 there is more or less vapor than state ①. Hence need to find  $x$  (if defined).

## Assumptions

Pure substance.  
ideal process.

## Laws

$$x = \frac{\text{Mass of Vapor}}{\text{total mass}} = \frac{m_g}{m_f + m_g} = \frac{\frac{V_g}{v_g}}{\frac{V_f}{v_f} + \frac{V_g}{v_g}}$$

$$v = \frac{V}{m}, \quad v = v_f + x(v_g - v_f)$$

## Steps

Find  $x_1$  ( $x$  in state ①).

in state 1

$$x_1 = \frac{V_g/v_g}{\frac{V_f}{v_f} + \frac{V_g}{v_g}} \quad \text{but } V_f = \frac{V_g}{10}$$

$$x_1 = \frac{10V_f/v_g}{\frac{V_f}{v_f} + 10V_f/v_g} = \frac{\frac{10}{v_g}}{\frac{1}{v_f} + \frac{10}{v_g}} = \boxed{\frac{10v_f}{v_g + 10v_f}} \rightarrow$$



so can find  $x_1$  if know  $v_f$  and  $v_g$ .

now use properties given in state ① to find  $v_f$  and  $v_g$ .

From table B.1.1, For  $T = T_1$  look up  $v_f$  and  $v_g$ .

now can find  $v_1$ :

$$v_1 = v_f + x_1 (v_g - v_f)$$

now in state ②. Since closed tank, hence Volume does not change. so  $v_2 = v_1$

Find  $x_2$  from  $v_1 = v_f + x_2 (v_g - v_f)$

$$\Rightarrow x_2 = \frac{v_1 - v_f}{v_g - v_f}$$

to find  $v_f, v_g$  in state ② use table B.1 again, since we are given  $P_2 = 2 \text{ MPa}$ .

now we have  $x_1$  and  $x_2$ , we can find if there is more or less Vapor.

if  $x_2 > x_1 \Rightarrow$  more Vapor in state ②

to find  $T_2$ , look up table B.1 again given  $P_2$ .



## Numerical

$$x_1 = \frac{10 v_f}{v_g + 10 v_f}$$

From Table B.1.1, For  $T = 100^\circ\text{C} \Rightarrow v_f = 0.001044 \text{ m}^3/\text{kg}$ .

$$v_g = 1.67290 \text{ m}^3/\text{kg}$$

$$\Rightarrow x_1 = \frac{10(0.001044)}{1.67290 + 10(0.001044)} = \boxed{0.0062019}$$

$$\text{So } v_1 = v_f + x_1(v_g - v_f)$$

$$= 0.001044 + 0.0062019(1.67290 - 0.001044)$$

$$= \boxed{0.011379 \text{ m}^3/\text{kg}}$$

state 2:

since closed vessel  $\Rightarrow v_2 = v_1 = 0.011379 \text{ m}^3/\text{kg}$ .

From table B.1.1, at  $P = 2 \text{ MPa}$ ,  $v_f < v_2 < v_g$

hence in state 2, still in mixed phase

$$v_f = 0.00177 \text{ m}^3/\text{kg}, \quad v_g = 0.09963 \text{ m}^3/\text{kg}$$

$$\text{So } x_2 = \frac{v_2 - v_f}{v_g - v_f} = \frac{0.011379 - 0.00177}{0.09963 - 0.00177}$$

$$= \boxed{0.10362}$$

hence  $x_2 > x_1 \Rightarrow$  Mass of Vapor in state ② is more than in state ①.

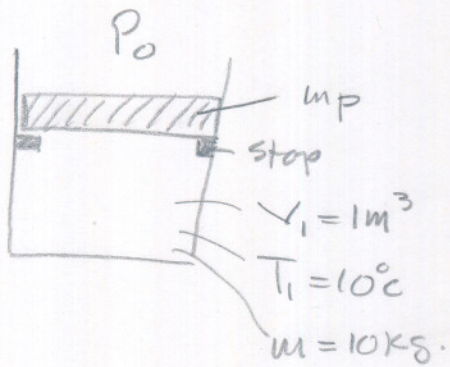
to Find  $T_2$ , since in mixed phase, again from B.1.1, we see that for  $P = 2 \text{ MPa}$ ,  $T_{\text{sat}} = \boxed{212.42^\circ\text{C}}$

Problem 3-63

10/16

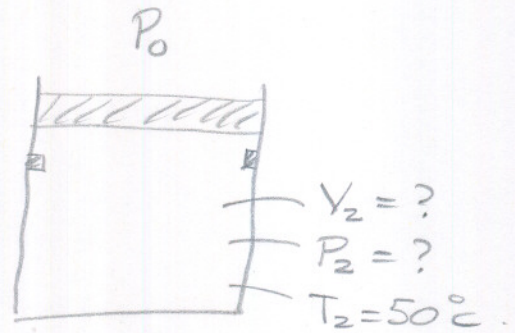
Statement

Ammonia at  $10^\circ\text{C}$  with mass  $10\text{kg}$  in a piston/cylinder assembly with initial volume of  $1\text{m}^3$ . Piston initially rests on the stops has mass such that a pressure of  $900\text{kPa}$  will float it. Now ammonia is slowly heated to  $50^\circ\text{C}$ . Find Final Pressure and Volume.



state ①

Process  
slow heating



state ②

in state ①, Piston is resting on stops. in state ② new temp. is  $50^\circ\text{C}$ . need to find Final Pressure and Final Volume.

assumptions

- Pure substance
- Frictionless Piston.
- ideal process

Laws

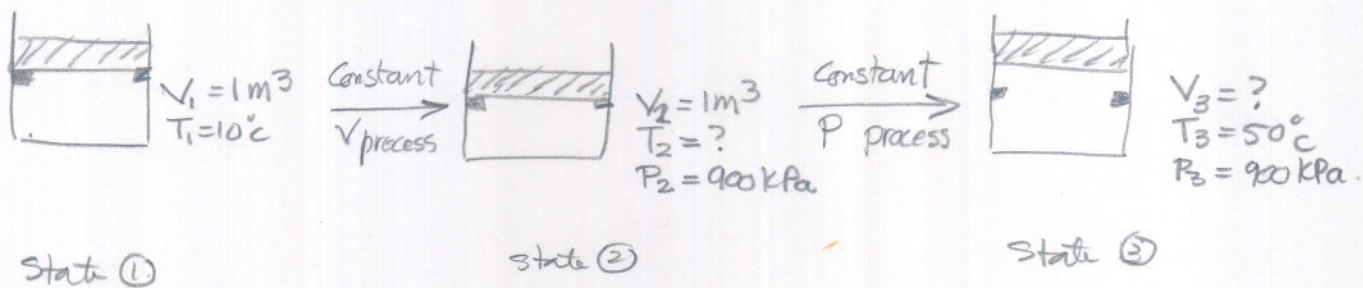
$v = \frac{V}{m}$

Steps

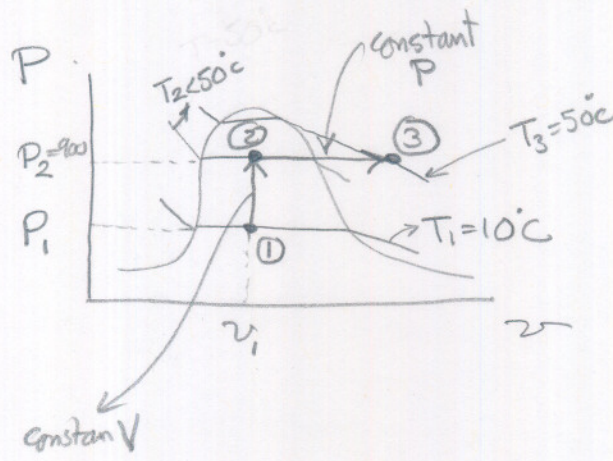


To reach Final state, Process can go via 2 different Paths. If final pressure  $< 900 \text{ kPa}$ , then Piston will not rise, and so this is a constant Volume Problem. But if, as we raise temp. pressure reaches  $900 \text{ kPa}$ , then Piston will start to rise, but Pressure will remain constant at this final P. until Final temp. reaches  $50^\circ \text{C}$ .

so problem looks as follows



So, if  $T_2 = 50^\circ \text{C}$ , then Process is only ①  $\rightarrow$  ②.  
 but if  $T_2 < 50^\circ \text{C}$ , the process is ①  $\rightarrow$  ②  $\rightarrow$  ③



①  $\rightarrow$  ②  $\rightarrow$  ③ process



$v_1 = \frac{V_1}{m}$  and knowing  $T_1$  we can find  $x_1$ , hence know phase

at state ②.  $v_2 = v_1$ . From table B.2.1. lookup  $T$  corresponding to  $P = P_{\text{stop}} = 900 \text{ kPa}$ .

if  $T_2 < T_{\text{final}}$ , then this is now a constant pressure process. use superheated ammonia table, lookup under  $P_{\text{final}}$  and  $T_{\text{final}}$  to find  $v_{\text{final}}$ .

Numerical

$$v_1 = \frac{V_1}{m} = \frac{1 \text{ (m}^3\text{)}}{10 \text{ (kg)}} = 0.1 \text{ m}^3/\text{kg}.$$

From B.2.1, at  $T_1 = 10^\circ\text{C}$ , we see  $v_1 < v_g$ .  
hence Saturated ammonia.

From same table, I see that for  $P = 900 \text{ kPa}$ ,  $T$  is between  $20^\circ\text{C}$  and  $25^\circ\text{C}$ , this means for  $T = 50^\circ\text{C}$ , we must be in superheated phase.

From table B.2.2, For  $P = 900 \text{ kPa}$ :

$$\text{For } P = 800 \text{ kPa, } T = 50^\circ\text{C} \rightarrow v = 0.18465 \text{ m}^3/\text{kg}.$$

$$P = 1000 \text{ kPa, } T = 50^\circ\text{C} \rightarrow v = 0.14499 \text{ m}^3/\text{kg}.$$

so interpolation to final at  $P = 900 \text{ kPa}$ :

$$\frac{1000 - 800}{0.14499 - 0.18465} = \frac{1000 - 900}{0.14499 - v}$$

$$200(0.14499 - v) = 100(0.14499 - 0.18465)$$

$$(200)(0.14499) - 200v = 14.499 - 18.465$$

$$v = \frac{(200)(0.14499) - (14.499 - 18.465)}{200} = \boxed{0.16482 \text{ m}^3/\text{kg}}$$

$$\text{so } v_2 = v_2 m = (0.16482)(10) = \boxed{1.6482 \text{ m}^3}$$

### Problem 3.75

statement given saturated R-134a at 3 different T,  
 $T_1 = -40^\circ\text{C}$ ,  $T_2 = 0^\circ\text{C}$ ,  $T_3 = +40^\circ\text{C}$ . need to Find specific  
19% volume at these Temps. Find % relative error =  
 $100(v - v_g) / v_g$  at each T.

### assumptions

ideal gas, R at  $25^\circ\text{C}$ , 100 kPa. in equilibrium.

### Laws

ideal gas law  $PV = mRT$ ,  $T(\text{K}) = 273.15 + T(\text{C})$

$$v = \frac{V}{m}$$

relative % error =  $100(v - v_g) / v_g$ .

### steps

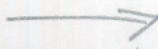
since we are told this is saturated R-134a, then  
use table B.5.1. For each given T, Find  
 $P_{\text{sat}}$ . then

$$v = \frac{V}{m} = \frac{RT}{P_{\text{sat}}}$$

Constant from table A.5  
given  
From Table B.5.1

now find % relative error, since we know  $v_g$  as  
well from table B.5.1.

### Numerical



From A.5,  $R = 0.08149 \text{ KJ/kg-K}$

T	$v_g \text{ (m}^3/\text{kg)}$	$P_{\text{sat}} \text{ (kPa)}$	$v = \frac{RT}{P_{\text{sat}}} \text{ (KJ/m}^3\text{)}$	% error
$-40^\circ\text{C}$	0.35696	51.8	$v = \frac{(0.08149)(273.15 - 40)}{51.8}$ $= 0.36678$	$\frac{100(0.36678 - 0.35696)}{0.35696}$ $= 2.751$
$0^\circ\text{C}$	0.06919	294.0	$v = \frac{(0.08149)(273.15)}{294.0}$ $= 0.07571$	$\frac{100(0.07571 - 0.06919)}{0.06919}$ $= 9.4233$
$40^\circ\text{C}$	0.02002	1017.0	$v = \frac{(0.08149)(273.15 + 40)}{1017.0}$ $= 0.02509$	$\frac{100(0.02509 - 0.02002)}{0.02002}$ $= 25.324$

notice that % error increases with temp. increase.

## Problem 3.92

10/16

### Statement

Find Phase, quality  $x$  if defined, and missing property  $P$  or  $T$ .

a)  $H_2O$ ,  $T = 120^\circ C$ ,  $v = 0.5 \text{ m}^3/\text{kg}$ .

b)  $H_2O$ ,  $P = 100 \text{ kPa}$ ,  $v = 1.8 \text{ m}^3/\text{kg}$ .

c)  $H_2O$ ,  $T = 263 \text{ K}$ ,  $v = 200 \text{ m}^3/\text{kg}$ .

### Assumptions

Pure substance. In equilibrium.

### Laws

Use thermodynamics tables.

Find  $x$  from  $v = v_f + x(v_g - v_f) \Rightarrow x = \frac{v - v_f}{v_g - v_f}$

IF  $v > v_g \Rightarrow$  superheated phase. IF  $v < v_f \Rightarrow$  compressed liquid.

### Steps

For each problem, lookup under table B.1.1 or B.1.2 values for  $v_f$  and  $v_g$ . Can find phase by comparing  $v$  to  $v_f, v_g$ .

Find missing property by lookup from appropriate table.

### Numerical

a). From B.1.1, for  $T = 120^\circ C$ ,  $v_f = 0.001060 \text{ m}^3/\text{kg}$ .

$v_g = 0.89186 \text{ m}^3/\text{kg}$ . Hence Mixed phase

Saturated water - saturated vapor.

$P_{\text{sat}} = 198.5 \text{ kPa}$  From B.1.1.  $x = \frac{0.5 - 0.00106}{0.89186 - 0.00106} = \boxed{0.56}$

b) From B.1.2, For  $P = 100 \text{ kPa}$ ,  $v_f = 0.001043 \text{ m}^3/\text{kg}$ ,

$v_g = 1.694 \text{ m}^3/\text{kg}$ . Here  $v > v_g \Rightarrow$  superheated

From B.1.3, For  $P = 100 \text{ kPa}$ ,  $v = 1.8$  do interpolation:

$$\frac{150 - 99.62}{1.93636 - 1.694} = \frac{150 - T}{1.93636 - 1.8}$$

$(150 - 99.62)(1.93636 - 1.8) = (150 - T) \Rightarrow T = \boxed{121.65449^\circ C}$



$x$  undefined since superheated.

c) For  $T = 263 - 273.15 = -10.15^\circ$ ,

Use B.1.5.  $\Rightarrow P = 0.2601 \text{ kPa}$  (used  $-10^\circ\text{C}$ ).

$v_f = 0.0010891$ ,  $v_g = 466.757 \text{ m}^3/\text{kg}$ .

hence  $v_g < v < v_g \Rightarrow$  Saturated solid - Saturated Vapor

$$x = \frac{v - v_f}{v_g - v_f} = \frac{200 - 0.0010891}{466.757 - 0.0010891} = \boxed{0.428487}$$

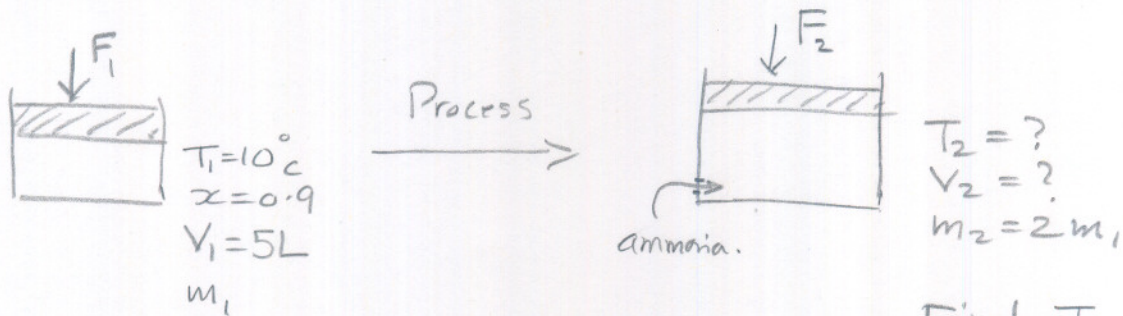
### Problem 3.104

statement

10/10

Cylinder with ammonia fitted with Piston restrained by external Force that is Proportional to cylinder Volume squared. in state ①,  $T = 10^\circ\text{C}$ ,  $x = 0.9$ ,  $V = 5\text{L}$ . A valve on cylinder is opened and additional ammonia flows into cylinder until mass is doubled.

If at this point  $P = 1.2\text{MPa}$ , Find Final  $T$ .



assumptions

Pure substance  
ideal Process.

Laws

$$F = K V^2$$

external Force  
↓  
Constant.

$$v = \frac{V}{m}, \quad v = v_f + x(v_g - v_f)$$

Steps

$$F = K V^2$$

$$\text{so } F_1 = K V_1^2 \Rightarrow K = \frac{F_1}{V_1^2}$$

$$\text{but to balance Piston, } F_1 = P_1 A$$

$$\text{hence } \boxed{K = \frac{P_1 A}{V_1^2}} \quad \text{--- ①}$$

Find  $P_1$  From Table B.2.1 For  $T_1 = 10^\circ\text{C}$

$$\text{now find } v_1 = v_f + x_1 (v_g - v_f)$$

$$\text{so we find } \boxed{m_1 = \frac{V_1}{v_1}} \quad \text{--- ②} \quad \rightarrow$$

now in state ②

balance forces for Piston:

$$F_2 = P_2 A$$

$$K V_2^2 = P_2 A$$

$$\text{so } V_2^2 = \frac{P_2 A}{K} \Rightarrow V_2 = \sqrt{\frac{P_2 A}{K}} \quad \text{--- (3)}$$

but from ①, substitute into ③ we get

$$V_2 = \sqrt{\frac{P_2 A}{P_1 A}} V_1^2 = \boxed{V_1 \sqrt{\frac{P_2}{P_1}}} \quad \text{--- (4)}$$

$$\text{so } v_2 = \frac{V_2}{m_2} = \frac{V_1 \sqrt{P_2/P_1}}{2 m_1} \quad \text{--- (5)}$$

so now we have  $P_2$  and  $v_2$  values we can find  $T_2$  from table B.2.1 or B.2.2.

### Numerical

From table B.2.1, For  $T_1 = 10^\circ\text{C}$ ,  $v_f = 0.0016 \text{ m}^3/\text{kg}$ .

$$v_g = 0.20541 \text{ m}^3/\text{kg}. \quad \boxed{P_1 = 615.2 \text{ kPa.}}$$

$$\text{so } v_1 = v_f + x_1 (v_g - v_f)$$

$$= 0.0016 + 0.9 (0.20541 - 0.0016) = \boxed{0.185029 \text{ m}^3/\text{kg}}$$

$$\text{From eq ② } m_1 = \frac{V_1}{v_1} = \frac{5 \times 10^{-3} \text{ (m}^3\text{)}}{0.185029 \text{ (m}^3/\text{kg)}} = \boxed{0.027 \text{ kg}}$$

$$\text{From eq ④ } V_2 = V_1 \sqrt{\frac{P_2}{P_1}} = 5 \times 10^{-3} \sqrt{\frac{1.2 \times 10^6}{615.2 \times 10^3}} = \boxed{0.006983 \text{ m}^3}$$

$$\text{so from eq ⑤ } v_2 = \frac{V_2}{m_2} = \frac{0.006983}{(0.027) \times 2} = \boxed{0.12935 \text{ m}^3/\text{kg}}$$

so for  $v_2, P_2$ : From B.2.2, interpolation (superheated since From B.2.1  $v > v_g$  for  $P=1.2 \text{ MPa}$ )

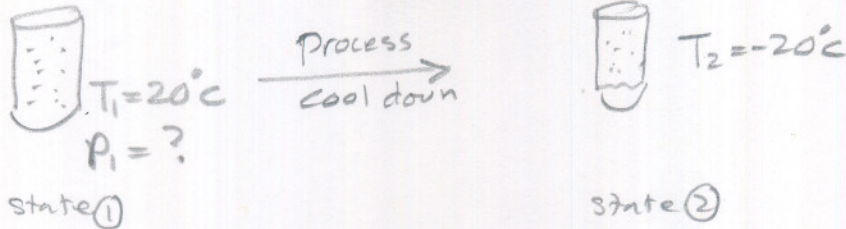
$$\frac{80-70}{0.13387-0.1289} = \frac{80-T_2}{0.13387-0.12935} \Rightarrow \boxed{T_2 = 70.9^\circ\text{C}}$$

Problem 3.110

12/10

Statement

Given sealed tube contain R-22 Vapor at 20°C. need to know P at this temp. tube cooled to -20°C, small droplets of liquid are observed on glass wall. Find initial pressure.



Assumptions

Pure substance. Ideal Process.

when droplets seen  $\Rightarrow v = v_g$  as starts of condensation.

Laws

use R-22 thermodynamics tables.

droplets/vapor  $\Rightarrow$  mixed phase.

Steps

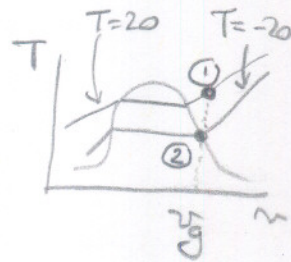
since droplets and vapor at  $T_2 \Rightarrow$  saturated mixed liquid-vapor phase.

hence use table B.4.1 to find  $v_g$ .

Since tube is sealed  $\Rightarrow$  constant v process.

hence use table B.4.2 (superheated phase)

using  $v_g$  found above and using  $T_1 = 20^\circ\text{C}$  to find  $P_2$ .



Numerical

From B.4.1, for  $T = -20^\circ\text{C}$ ,  $v_g = \boxed{0.09284 \text{ m}^3/\text{kg}}$

From B.4.2, for  $T = 20^\circ\text{C}$  and  $v_g = \uparrow$  Find P

I see for  $P = 300 \text{ kPa}$ ,  $T = 20^\circ\text{C}$ ,  $\Rightarrow v = 0.08947 \text{ m}^3/\text{kg}$

for  $P = 200 \text{ kPa}$ ,  $T = 20^\circ\text{C}$ ,  $\Rightarrow v = 0.13651 \text{ m}^3/\text{kg}$

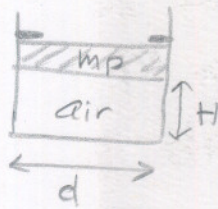
So interpolation:

$$\frac{300 - 200}{0.08947 - 0.13651} = \frac{300 - P}{0.08947 - 0.09284} \Rightarrow \boxed{P = 292.83 \text{ kPa}}$$

### Problem 3.111

statement

given



$$P_1 = 250 \text{ kPa}$$

$$T_1 = 300^\circ\text{C}$$

$$H = 25 \times 10^{-2} \text{ m}$$

$$d = 0.1 \text{ m}$$

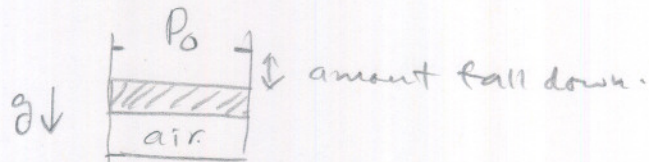
$$m_p = 50 \text{ kg}$$

9/10 State ①

atmosphere at  $20^\circ\text{C}$ . Piston in state ① above originally pushed against stops.

Cylinder is cooled down.

- Find at what  $T$  piston begins to move down?
- How far does it fall down when air temp reaches ambient?



-1 Draw Diagram

Final state. (state ②)

### assumptions

ideal gas. so can use  $PV = mRT$ .

assume frictionless piston.

ideal Process

### Laws

ideal gas law.  $PV = mRT$

### Steps

- Piston begins to fall down when air pressure inside cylinder just large enough to support weight of piston.

so From Piston balance Forces, we set

$$P_0 A + m_p g = P A$$

$$\Rightarrow \boxed{P = \frac{P_0 + \frac{m_p g}{A}}{1}} \quad \text{--- (1) ---} \rightarrow$$

From ideal gas law

$$PV = nRT.$$

so From ① into above, we set

$$\left(P_0 + \frac{m_p g}{A}\right) V = nRT$$

$$\text{or } T = \left(P_0 + \frac{m_p g}{A}\right) \frac{V}{nR}$$

$$\text{but } V = AH$$

$$\text{so } T = \left(P_0 + \frac{m_p g}{A}\right) \frac{AH}{nR} \quad \text{--- ②}$$

to find  $m$  (mass of air inside cylinder), use initial state.

$$P_1 V_1 = nRT_1 \Rightarrow m = \frac{P_1 V_1}{RT_1} = \frac{P_1 AH}{RT_1} \quad \text{--- ③}$$

sub ③ into ②:

$$T = \left(P_0 + \frac{m_p g}{A}\right) \frac{AH \cancel{RT_1}}{P_1 AH \cancel{R}} = \boxed{\left(P_0 + \frac{m_p g}{A}\right) \frac{T_1}{P_1}} \quad \text{--- ④}$$

the above give the temp. when pistons begin to move down.

b) to find how far piston falls down, need to find final volume. call it  $V_2$ .

$$\text{From ideal gas law: } P_2 V_2 = nRT_2$$

$$\text{so } V_2 = \frac{nRT_2}{P_2}. \quad \text{but } n \text{ is same as from eq ③.}$$

and  $T_2$  is given as ambient temp.  $P_2$  is pressure to support piston, here same as eq ①. hence  $\rightarrow$

$$V_2 = \frac{P_1 A H}{R T_1} R T_2 = \boxed{\frac{P_1 A^2 H T_2}{A T_1 P_0 + T_1 m_p g}} \quad (5)$$

so  $\Delta h = \frac{V_1 - V_2}{A}$

↑ state ①  
state ②

Numerical

a) From eq (4)

$$T = \left( P_0 + \frac{m_p g}{A} \right) \frac{T_1}{P_1} = \left( 100 \times 10^3 + \frac{(50)(9.81)}{\pi \frac{0.1^2}{4}} \right) \frac{(273+300)}{250 \times 10^3}$$

$$= 372.3409 \text{ K}$$

$$= \boxed{99.34 \text{ } ^\circ\text{C}}$$

b) From eq (5)

$$V_2 = \frac{P_1 A^2 H T_2}{A T_1 P_0 + T_1 m_p g} = \frac{(250 \times 10^3) \left[ \pi \frac{0.1^2}{4} \right]^2 (25 \times 10^{-2}) (273+20)}{\left( \pi \frac{0.1^2}{4} \right) (273+300) (100 \times 10^3) + (273+300) 50 \times 9.81}$$

$$= 1.5451 \times 10^{-3} \text{ m}^3 = 1.545 \text{ L}$$

hence  $\Delta h = \frac{\Delta V}{A} \Rightarrow \Delta h = \frac{V_1 - V_2}{A} = \frac{A H - V_2}{A}$

$$= \frac{\left( \pi \frac{0.1^2}{4} \right) (25 \times 10^{-2}) - 1.5451 \times 10^{-3}}{\pi \frac{0.1^2}{4}} = 0.05327 \text{ m}$$

So piston Falls down by  $\boxed{5.327 \text{ cm}}$