

HW 8  
Electronic Communication Systems  
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California State University, Fullerson

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## 1 Questions

EE 443

Lect 3

HW # 8

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Dm 3.4)

$$V_2 = a_1 V_1(t) + a_2 V_1^2(t) \quad (1)$$

where,  $V_1(t) = A_c \cos 2\pi f_c t + m(t) \quad (2)$

subst. eq. (2) into eq (1)

$$V_2(t) = a_1 [A_c \cos 2\pi f_c t + m(t)] + a_2 [A_c \cos 2\pi f_c t + m(t)]^2$$

$$\Rightarrow V_2(t) = \underbrace{a_1 A_c \left[ 1 + \frac{2a_2}{a_1} m(t) \right] \cos 2\pi f_c t}_{\text{AM Signal}} + a_1 m(t) + a_2 m^2(t) + a_2 A_c^2 \underbrace{\cos^2(2\pi f_c t)}_{\frac{1}{2}[1 + \cos 4\pi f_c t]}$$

The signal at the output of bandpass filter is:

$$V_o(t) = a_1 A_c \left[ 1 + \frac{2a_2}{a_1} m(t) \right] \cos 2\pi f_c t$$

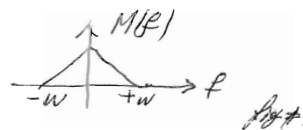
which is an AM wave.

## 2 Key solution

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 Drill Prob. # 3, 4)  $V_2(t) = a_1 v_1(t) + a_2 v_1^2(t)$  (1),  $v_1(t) = A_c \cos(2\pi f_c t) + m(t)$  (2)

$$V_2(t) = a_1 A_c \cos(2\pi f_c t) + a_1 m(t) + a_2 A_c^2 \cos^2(2\pi f_c t) + a_2 m^2(t) + 2 a_2 A_c m(t) \cos(2\pi f_c t) \quad (3)$$

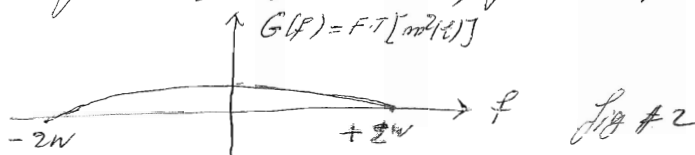
Assume  $M(f)$  has the following form:



Let  $g(t) \equiv m^2(t) = m(t) \cdot m(t)$

$\Rightarrow G(f) = M(f) \otimes M(f)$  The spectrum of  $g(t) = m^2(t)$

will extend from  $-2W$  to  $2W$  Hz, for example would be



Note: If you want to find  $G(f)$ , then you have

to do  $G(f) = \int_{-\infty}^{+\infty} M(\lambda) M(f-\lambda) d\lambda$ . We are not interested to find the exact equation of  $G(f)$ , all we need to know is that the spectrum of  $G(f) = F.T[m^2(t)]$  will extend from  $-2W$  to  $2W$  Hz.

Let us to take the F.T of eq(3) and plot it!

$$V_2(t) = a_1 A_c \cos(2\pi f_c t) + a_1 m(t) + \frac{a_2 A_c^2}{2} [1 + \cos(4\pi f_c t)] + a_2 m^2(t) + 2 a_2 A_c m(t) \cos(2\pi f_c t) \quad (4)$$

$$\Rightarrow V_2(f) = \frac{a_1 A_c}{2} [\delta(f-f_c) + \delta(f+f_c)] + a_1 M(f) + \frac{a_2 A_c^2}{2} \delta(f) + \frac{a_2 A_c^2}{4} [\delta(f-2f_c) + \delta(f+2f_c)] + a_2 \underbrace{F.T[m^2(t)]}_{G(f)} + a_2 A_c [M(f-f_c) + M(f+f_c)] \quad (5)$$

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The plot of eq. (5) is shown in Figure # 3.

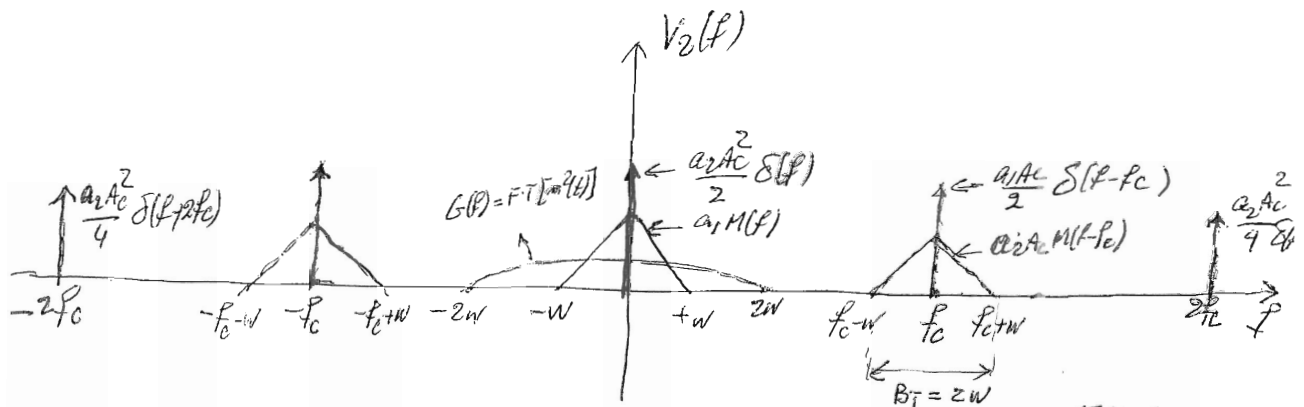


Fig # 3

Fig # 3 shows the spectral content of  $V_2(t)$ .

1) To extract the desired AM signal, use eq (4) and identify the AM signal:

$$V_2(t) = \underbrace{a_1 A_c \left[ 1 + \frac{2a_2}{a_1} m(t) \right] \cos 2\pi f_c t}_{\text{Desired AM signal}} + \underbrace{\left( a_1 m(t) + a_2 m^2(t) + \frac{a_2 A_c^2}{2} \cos 4\pi f_c t \right)}_{\text{Undesired component}} \quad (6)$$

A Bandpass filter centered at  $f_c$  with total extend of  $2w/2$ , that is having a transfer function of:

$$H(f) = \text{rect}\left(\frac{f-f_c}{2w}\right) + \text{rect}\left(\frac{f+f_c}{2w}\right) \quad (7)$$

will pass the desired signal (AM signal) and eliminated the unwanted components.

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Using eq. (7) and figure # (3) we see that the required B.P.F must have a bandwidth of  $2W$  Hz and centered at  $f_c$ , thus the cut-off frequencies of BPF are  $f_c - W$  and  $f_c + W$  Hz.

c) To avoid spectral overlapping of the desired signal (AM signal) with that of unwanted signals in  $v_d(t)$ , using figure # 3, we see that

$$\left. \begin{array}{l} 1) f_c - W \geq 2W \Rightarrow f_c \geq 3W \\ 2) f_c + W \leq 2f_c \Rightarrow f_c \geq W \end{array} \right\} \text{Thus } f_c \geq 3W$$

### 3.23

Assume  $m(t)$  with spectrum of

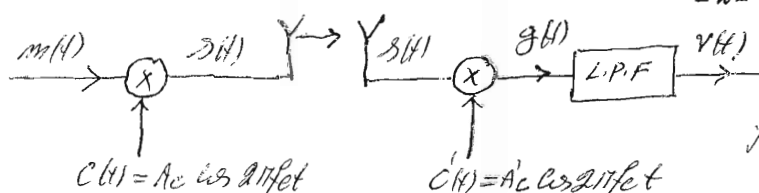
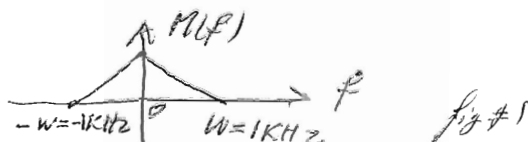


fig # (2) Coherent detection of DSB-SC.

$$s(t) = m(t) \cdot c(t) = A_c m(t) \cos 2\pi f_c t \Rightarrow S(f) = \frac{A_c}{2} [M(f-f_c) + M(f+f_c)] \quad (1)$$

$$g(t) = s(t) \cdot c'(t) = A_c A_c' m(t) \cos^2 2\pi f_c t = \frac{A_c A_c'}{2} m(t) [1 + \cos 4\pi f_c t] \quad (2)$$

$$G(f) = \frac{A_c A_c'}{2} M(f) + \frac{A_c A_c'}{4} [M(f-2f_c) + M(f+2f_c)] \quad (3)$$

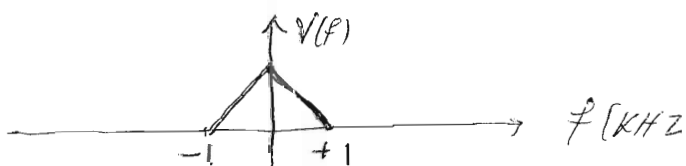
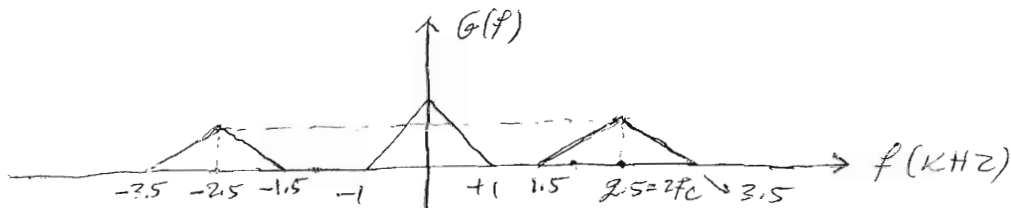
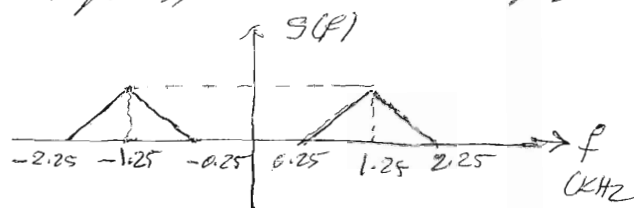
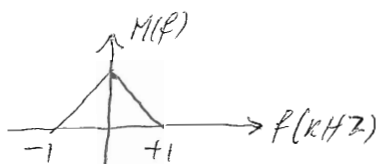
a) For  $f_c = 1.25$  KHz, the spectrum of  $m(t)$ , the spectrum of  $s(t)$  and the spectrum of  $v(t)$  (detector output) are?

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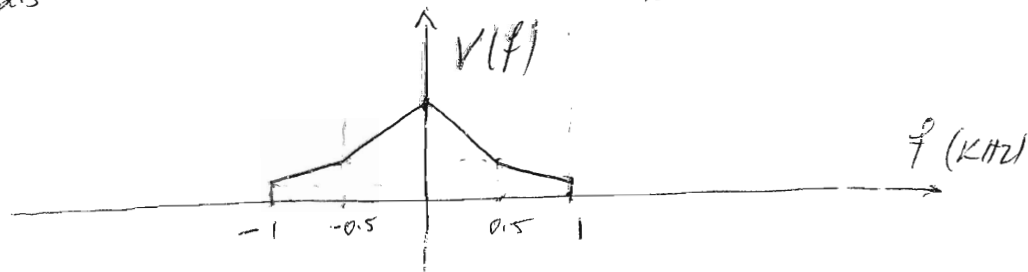
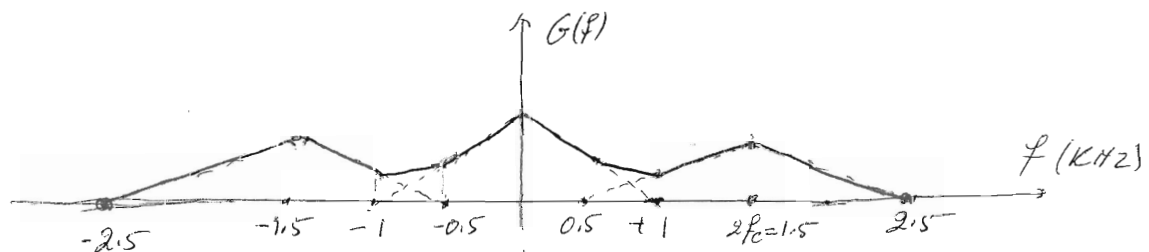
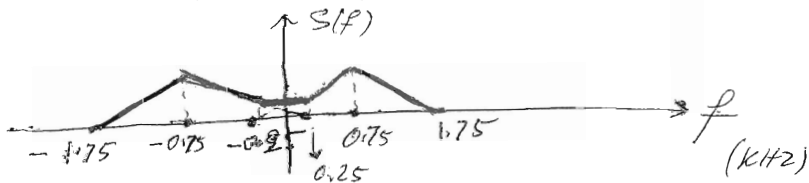
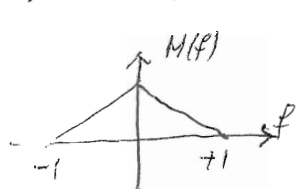
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b) For  $f_c = 0.75$  KHz, the respective spectra are :



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Problem 5-1

AM broadcast transmitter is tested by feeding RF output into  $50\text{-}\Omega$  load. Tone Modulation is used. Carrier frequency is  $850\text{ kHz}$  and power output is  $5000\text{ W}$ . The sinusoidal tone of  $1000\text{ Hz}$  is set for  $90\%$  modulation.

- Evaluate the FCC Power in dBK (dB over 1 kW) units.
- Write an equation for the voltage that appears across the  $50\text{-}\Omega$  load, giving numerical values for all constants.
- Sketch the spectrum of this voltage as it would appear on a calibrated spectrum analyzer.
- What is the average power that is being dissipated in the dummy load?
- What is peak envelope power?

Answer

a)  $10 \log_{10} \left( \frac{5000}{1000} \right) = 6.9897 \approx \boxed{7 \text{ dBK}}$

b)  $s(t) = A_c (1 + m \cos(\omega_m t)) \cos(\omega_c t)$  ——— ①

Where  $\omega_m$  is the tone frequency  $2\pi(1000)$  rad/sec.  
and  $\omega_c$  is the carrier frequency  $2\pi(850,000)$  rad/sec.  
 $m = .9$ . Need to find  $A_c$ :

Carrier Power =  $\frac{A_c^2}{2}$  ... but this is normalized to  $1\text{-}\Omega$ .

hence  $\boxed{P = \left( \frac{A_c^2}{2} \right) \frac{1}{R}}$  where  $R = 50\text{-}\Omega$ .

so  $P = \frac{A_c^2}{100} = A_c = \sqrt{100(P)}$  ... but  $P = 5000\text{ Watt}$

so  $A_c = \sqrt{100(5000)} = \boxed{707.1 \text{ V}}$

So voltage equation is ① given by

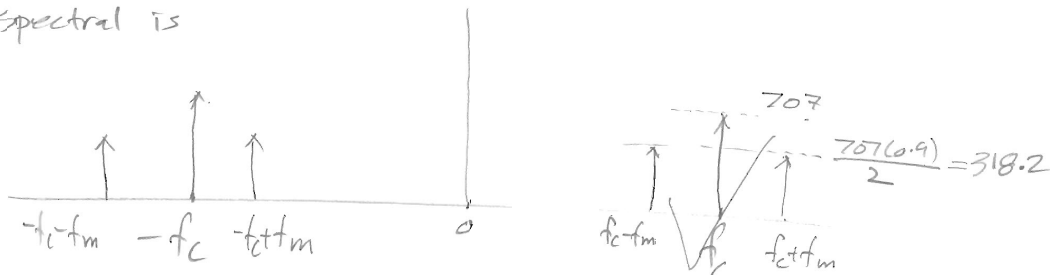
$s(t) = 707 (1 + 0.9 \cos(2\pi \times 1000)t) \cos(2\pi \times 850,000)t$





$$s(t) = 707 \cos 2\pi f_c t + \frac{707(0.9)}{2} [\cos(2\pi(f_c + f_m)t) + \cos(2\pi(f_c - f_m)t)]$$

hence spectral is



where  $f_c = 850 \text{ KHz}$   
 $f_m = 1 \text{ KHz}$

so  $f_c + f_m = 851 \text{ KHz}$   
 $f_c - f_m = 849 \text{ KHz}$

(d) The Total Normalized average power =  $\left(\frac{A_c^2}{2}\right) + \left(\frac{A_c \mu}{2}\right)^2$

hence, we  $R=50$ , we obtain

$$P_{av. \text{ in } R} = \frac{1}{R} \left[ \frac{A_c^2}{2} + \frac{A_c^2 \mu^2}{4} \right]$$

$$= \frac{1}{50} \left[ \frac{707^2}{2} + \frac{707^2 (0.9)^2}{4} \right] = \boxed{7,022.87 \text{ Watt}}$$

(e)  $A_{max} = A_c(1+\mu)$

hence Peak Power (average) is  $\frac{[A_c(1+\mu)]^2}{2} \times \frac{1}{R}$

$$= \frac{(707(1+0.9))^2}{2 \times 50} = \boxed{18,044.5 \text{ Watt}}$$

Normalized PEP =  $\frac{[707(1+0.9)]^2}{2} = \boxed{902,227 \text{ watt}}$  this is not Normalized.

5-3

AM transmitter modulated with  $m(t) = 0.2 \sin \omega_1 t + 0.5 \cos \omega_2 t$

$f_1 = 500 \text{ Hz}$ ,  $f_2 = 500\sqrt{2} \text{ Hz}$ .  $A_c = 100$ .

- (a) Evaluate average power of the AM signal  
 (b) Evaluate Peak Envelope Power (PEP).

Answer

(a) average power (normalized) is given by

$$\frac{A_c^2}{2} + \left(\frac{A_c \mu}{2}\right)^2$$

$$\begin{aligned} s(t) &= A_c (1 + \underbrace{0.2 \sin \omega_1 t + 0.5 \cos \omega_2 t}_{\text{expands } \Rightarrow \text{ sinusoid } f.}) \\ &= A_c \cos \omega_c t + \underbrace{2A_c \sin \omega_1 t + 0.5A_c \cos \omega_2 t}_{\text{another } \Rightarrow \text{ sin. } f.} \end{aligned}$$

so normalized average power

$$\begin{aligned} &\frac{A_c^2}{2} + \frac{(2A_c)^2}{2} + \frac{(0.5A_c)^2}{2} \\ &= \frac{100^2}{2} + \frac{20^2}{2} + \frac{50^2}{2} = \boxed{6,450 \text{ Watt}} \end{aligned}$$

When using load  $R = 50 \Omega$  given in problem 5-2, we obtain

$$\frac{6450}{50} = \boxed{129 \text{ Watt}} \quad \checkmark$$

(b)  $A_{max} = A_c(1 + \mu)$

$$\begin{aligned} \text{hence PEP} &= \frac{[100(1+2)]^2}{2} + \frac{[100(1+5)]^2}{2} \\ &= 7,200 + 11,250 = \boxed{18,450 \text{ Watt}} \end{aligned}$$

PEP over load of  $50 \Omega$ , we obtain

$$\text{PEP} = \frac{[100(1.2)]^2}{2 \times 50} + \frac{[100(1.5)]^2}{2 \times 50} = \boxed{369 \text{ Watt}} \quad \checkmark$$

5-7

A DSB-SC signal is modulated by  $w(t) = \cos \omega_c t + 2 \cos 2\omega_c t$

where  $f_c = 5000 \text{ Hz}$  and  $A_c = 1$ .

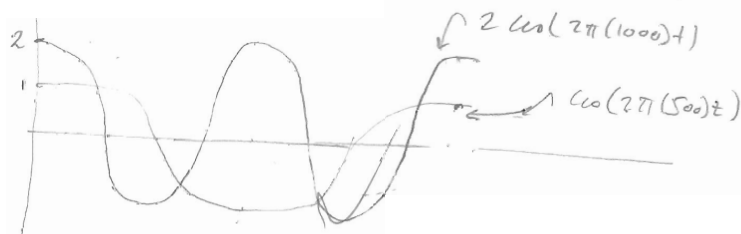
- write expression for DSB-SC signal and sketch picture of this waveform
- Evaluate and sketch the spectrum of this signal.
- Find the average (normalized) power
- Find PEP (normalized).

Answer

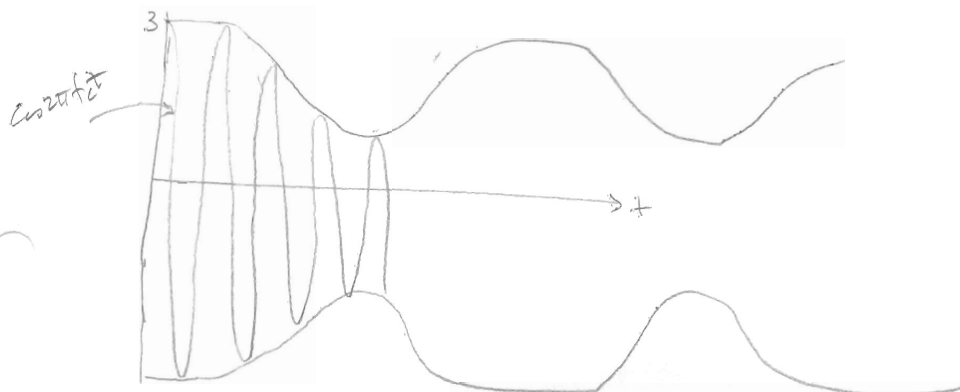
DSB-SC is double sided carrier suppressed.

$$a) \boxed{s(t) = A_c \cos \omega_c t w(t)}$$

$$\begin{aligned} \text{hence } s(t) &= \cos 2\pi f_c t (\cos \omega_c t + 2 \cos 2\omega_c t) \\ &= \cos 2\pi f_c t (\underbrace{\cos 2\pi(500)t + 2 \cos(2\pi(1000)t)}_{a(t)}) \end{aligned}$$



add these  
2 signals  $\Rightarrow$   
and multiply by carrier

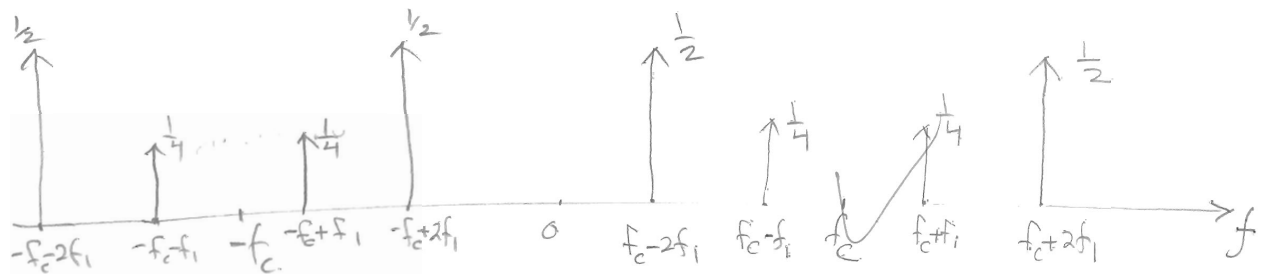


$\rightarrow$

$$\begin{aligned}
 b) \quad s(t) &= \cos 2\pi f_c ( \cos 2\pi f_1 t + 2 \cos 2\pi 2f_1 t ) \\
 &= \cos 2\pi f_c \cos 2\pi f_1 t + 2 \cos 2\pi f_c \cos 4\pi f_1 t \\
 &= \frac{1}{2} ( \cos 2\pi (f_c + f_1) t + \cos 2\pi (f_c - f_1) t ) \\
 &\quad + ( \cos 2\pi (f_c + 2f_1) t + \cos 2\pi (f_c - 2f_1) t ) \quad \text{--- (1)}
 \end{aligned}$$

$$\begin{aligned}
 \therefore s(t) &= \frac{1}{2} \cdot \left[ \frac{1}{2} ( \delta(f + f_c + f_1) + \delta(f - f_c - f_1) ) \right. \\
 &\quad \left. + \frac{1}{2} ( \delta(f + f_c - f_1) + \delta(f - f_c + f_1) ) \right] \\
 &\quad + \frac{1}{2} ( \delta(f + f_c + 2f_1) + \delta(f - f_c - 2f_1) ) \\
 &\quad + \frac{1}{2} ( \delta(f + f_c - 2f_1) + \delta(f - f_c + 2f_1) )
 \end{aligned}$$

$$\begin{aligned}
 &= \frac{1}{4} \delta(f + f_c + f_1) + \frac{1}{4} \delta(f - f_c - f_1) + \frac{1}{4} \delta(f + f_c - f_1) + \frac{1}{4} \delta(f - f_c + f_1) \\
 &\quad + \frac{1}{2} \delta(f + f_c + 2f_1) + \frac{1}{2} \delta(f - f_c - 2f_1) + \frac{1}{2} \delta(f + f_c - 2f_1) + \frac{1}{2} \delta(f - f_c + 2f_1)
 \end{aligned}$$



(c) Average power: From (1) using Formula  $\frac{\text{Amplitude}^2}{2}$  per tone:

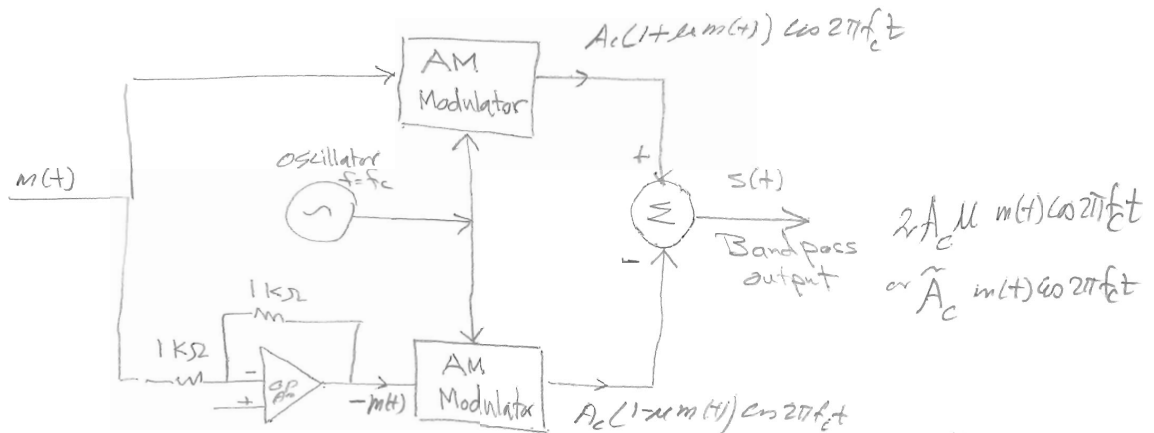
$$\frac{0.5^2}{2} + \frac{0.5^2}{2} + \frac{1^2}{2} + \frac{1^2}{2} = \frac{1}{8} + \frac{1}{8} + \frac{1}{2} + \frac{1}{2} = \boxed{1.25 \text{ Watt}}$$

(d)  $A_{\max} = A_c + \mu$ .  $n=2$  for the signal,  $\cos 2\pi f_c t + 2 \cos 2\pi f_1 t$   
 hence  $A_{\max} = 1 + 2 = \boxed{3}$

$$\therefore \text{PEP} = \frac{A_{\max}^2}{2} = \frac{9}{2} = \boxed{4.5 \text{ watt}}$$

5-9 A DSB-SC signal can be generated from 2 AM signals. Using mathematics to describe signals at each point on figure, prove output is DSB-SC.

Answer



∴ AM acts as an inverting Amplifier



$$V_{out} = -V_{in} \left( \frac{R_f}{R_{in}} \right)$$

since  $R_f = R_{in}$  in this problem, then  $V_{out} = -V_{in}$ .

$$\text{hence } S(t) = A_c(1+\mu m(t))\cos 2\pi f_c t - [A_c(1-\mu m(t))\cos 2\pi f_c t]$$

or

$$\begin{aligned} S(t) &= A_c \cos 2\pi f_c t + A_c \mu m(t) \cos 2\pi f_c t - [A_c \cos 2\pi f_c t - A_c \mu m(t) \cos 2\pi f_c t] \\ &= 2A_c \mu m(t) \cos 2\pi f_c t \end{aligned}$$

combine  $2A_c \mu \Rightarrow \tilde{A}_c$

$$\tilde{A}_c m(t) \cos 2\pi f_c t$$

we obtain equation for DSB-SC

hence the above circuit suppresses the carrier part.



$$\lim_{\omega \rightarrow \infty} \int_{-\infty}^{\infty} a_1 e^{-\alpha_1 \tau} e^{j2\pi f \tau} d\tau = a_1 \int_{-\infty}^{\infty} e^{-\alpha_1 \tau} e^{j2\pi f \tau} d\tau$$

$$a_1 \int_{-\infty}^{\infty} e^{-\alpha_1 \tau} e^{j2\pi f \tau} d\tau = \frac{a_1}{-j2\pi f + \alpha_1}$$

$$= \frac{a_1}{-j2\pi f + \alpha_1} (1) = \boxed{\frac{a_1}{-j2\pi f + \alpha_1}}$$

$$\text{and } \int_{-\infty}^{\infty} a_2 e^{-\alpha_2 \tau} e^{j2\pi f \tau} d\tau = \boxed{\frac{a_2}{-j2\pi f + \alpha_2}}$$

$$\text{and } \int_0^{\infty} a_1 e^{-\alpha_1 \tau} e^{j2\pi f \tau} d\tau = a_1 \int_0^{\infty} e^{\tau(-\alpha_1 - j2\pi f)} d\tau$$

$$= a_1 \frac{[e^{\tau(-\alpha_1 - j2\pi f)}]_0^{\infty}}{-\alpha_1 - j2\pi f} = \frac{a_1}{-\alpha_1 - j2\pi f} (-1) = \boxed{\frac{a_1}{\alpha_1 + j2\pi f}}$$

$$\text{and } \int_0^{\infty} a_2 e^{-\alpha_2 \tau} e^{-j2\pi f \tau} d\tau = \boxed{\frac{a_2}{\alpha_2 + j2\pi f}}$$

$$\text{hence } \boxed{S_Z(f) = \frac{a_1}{\alpha_1 - j2\pi f} + \frac{a_2}{\alpha_2 - j2\pi f} + \frac{a_1}{\alpha_1 + j2\pi f} + \frac{a_2}{\alpha_2 + j2\pi f}}$$

This can be simplified more as follows.

$$S_Z(f) = \frac{a_1 (\alpha_1 + j2\pi f) + a_1 (\alpha_1 - j2\pi f)}{(\alpha_1 - j2\pi f) (\alpha_1 + j2\pi f)} + \frac{a_2 (\alpha_2 + j2\pi f) + a_2 (\alpha_2 - j2\pi f)}{(\alpha_2 - j2\pi f) (\alpha_2 + j2\pi f)}$$

$$= \boxed{\frac{2a_1\alpha_1}{\alpha_1^2 + 4\pi^2 f^2} + \frac{2a_2\alpha_2}{\alpha_2^2 + 4\pi^2 f^2}}$$